

**OPTIMAL CONTROL OF A SPIN SYSTEM
ACTING ON A SINGLE QUANTUM BIT**

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Abstract: We study a quantum spin system acting on a single quantum bit. The evolution of this system is governed by the Schrödinger equation which takes the form of a right-invariant system on the special unitary group $SU(2)$ with two control inputs. Using a suitable version of Pontryagin's Principle which is tailor-made for control problems on Lie groups, the optimal controls are derived in two cases: the energy-optimal case (in which the control effort is minimized for a specified end time) and the time-optimal case (in which the control duration is minimized for given constraints on the size of the controls).

Keywords: Nonlinear control, optimal control, quantum spin systems.

Problem Formulation

The evolution of the spin system we want to consider is given by the Schrödinger equation

$$(1) \quad \dot{U}(t) = (c(t)A + u(t)X + v(t)Y)U(t)$$

where

$$(2) \quad A := \begin{bmatrix} i & 0 \\ 0 & -i \end{bmatrix}, \quad X := \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}, \quad Y := \begin{bmatrix} 0 & i \\ i & 0 \end{bmatrix}$$

and where c , u and v are functions of time describing the temporal variations of the external field. In our case we shall treat $t \mapsto u(t)$ and $t \mapsto v(t)$ as control functions whereas c is a constant (so that cA is a drift term in the system dynamics). Our goal will be to steer the system state from a given value $U(0)$ at time $t = 0$ to a specified value $U(\tau)$ at time $\tau > 0$ in such a way that a cost functional of the form

$$(3) \quad \int_0^\tau \Phi(u(t), v(t)) dt$$

(depending only on the controls, not on the state) becomes minimal. In applications one is mainly interested in the time-optimal case (in which $\Phi(u, v) \equiv 1$) either under the constraints $|u| \leq 1$ and $|v| \leq 1$ or under the more severe constraint $u^2 + v^2 \leq 1$. However, we shall also

discuss the case $\Phi(u, v) = (1/2)(u^2 + v^2)$ (with no constraints on u and v), in which the optimal controls can be found rather easily. This case can then be compared to the time-optimal case, as follows: Determine (analytically, if possible) the optimal controls $t \mapsto u(t; \tau)$ and $t \mapsto v(t; \tau)$ in dependence on the given duration τ and find the minimal τ which is compatible with the constraints imposed in the time-optimal case.

Lie-theoretic structure

Equation (1) is a control system evolving on the group $SU(2)$ of all complex (2×2) -matrices U such that $U^*U = \mathbf{1}$ and $\det(U) = 1$; equivalently,

$$(4) \quad SU(2) = \left\{ \begin{bmatrix} a & -\bar{c} \\ c & \bar{a} \end{bmatrix} \mid a, c \in \mathbb{C}, |a|^2 + |c|^2 = 1 \right\}.$$

Note that the system (1) is right-invariant in the sense that if $t \mapsto U(t)$ is a trajectory of (1) then so is $t \mapsto U(t)B$ for any fixed $B \in SU(2)$. (This, by the way, ensures that we can always assume that $U(0) = \mathbf{1}$; otherwise we can replace U by $U(t)U(0)^{-1}$, which satisfies the same equation as U .) The Lie algebra $\mathfrak{su}(2)$ of $SU(2)$ consists of all traceless skew-Hermitian (2×2) -matrices; it is spanned by the elements A , X and Y in (2), and these satisfy the bracket relations

$$(5) \quad [A, X] = -2Y, \quad [A, Y] = 2X, \quad [X, Y] = -2A.$$

For later purposes, we give an explicit formula for the exponential function of $\mathfrak{su}(2)$. Given a matrix

$$(6) \quad M = \begin{bmatrix} ic & -\bar{z} \\ z & -ic \end{bmatrix} \in \mathfrak{su}(2) \quad (c \in \mathbb{R}, z \in \mathbb{C})$$

we let

$$(7) \quad S := \begin{bmatrix} \bar{z} & \bar{z} \\ i(c-\Delta) & i(c+\Delta) \end{bmatrix} \text{ where } \Delta := \sqrt{c^2 + |z|^2}$$

and observe that

$$(8) \quad S^{-1}MS = \begin{bmatrix} i\Delta & 0 \\ 0 & -i\Delta \end{bmatrix} =: D$$

so that $M = SDS^{-1}$ and hence $\exp(tM) = S \exp(tD) S^{-1}$ for all $t \in \mathbb{R}$. Explicitly, the last equation reads

$$(9) \quad \begin{aligned} \exp\left(t \begin{bmatrix} ic & -\bar{z} \\ z & -ic \end{bmatrix}\right) &= \\ \frac{1}{\Delta} \begin{bmatrix} \Delta \cos(t\Delta) + ic \sin(t\Delta) & -\bar{z} \sin(t\Delta) \\ z \sin(t\Delta) & \Delta \cos(t\Delta) - ic \sin(t\Delta) \end{bmatrix} & \\ = \cos(t\Delta) \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \frac{\sin(t\Delta)}{\Delta} \begin{bmatrix} ic & -\bar{z} \\ z & -ic \end{bmatrix}. & \end{aligned}$$

Note that (9) simply says that

$$(10) \quad \exp(tM) = \cos(t\sqrt{\det(M)}) \mathbf{1} + \frac{\sin(t\sqrt{\det(M)})}{\sqrt{\det(M)}} M.$$

This formula could also have been derived from the Hamilton-Cayley Theorem $M^2 - (\text{tr } M)M + (\det M)\mathbf{1} = \mathbf{0}$ which, because of $\text{tr}(M) = 0$, becomes $M^2 = -\det(M)\mathbf{1}$. Consequently, we find that $M^{2k} = (-\det(M))^k \mathbf{1}$ and $M^{2k+1} = (-\det(M))^k M$ for all $k \in \mathbb{N}_0$; plugging these equations into the expansion $\exp(tM) = \sum_{r=0}^{\infty} t^r M^r / r!$, equation (10) follows.

We now exploit the Lie-theoretic structure inherent in the problem by invoking a version of Pontryagin's Maximum Principle which is tailor-made for right-invariant systems on Lie groups. This version states that, if u and v are optimally chosen, then there is an absolutely continuous function $p : [0, \tau] \rightarrow \mathfrak{su}(2)$ satisfying the adjoint equation

$$(11) \quad \dot{p}(t) = -p(t) \circ \text{ad}(cA + u(t)X + v(t)Y)$$

and never becoming zero, which is such that $u(t)$ and $v(t)$ minimize the Hamiltonian

$$(12) \quad H = \chi \cdot \Phi(u, v) + c \cdot p(t)A + u \cdot p(t)X + v \cdot p(t)Y$$

(where $\chi \in \{0, 1\}$) with respect to u and v almost everywhere; moreover, the Hamiltonian is constant along the optimal trajectory and control, the constant being zero if the final time τ is not fixed beforehand. (The abnormal

case $\chi = 0$ will not be of significance in the problems at hand.) Applying (11) to A , X and Y , respectively, and using the bracket relations (5) we obtain the equations

$$(13) \quad \begin{aligned} \dot{p}(t)A &= -p(t)(2u(t)Y - 2v(t)X), \\ \dot{p}(t)X &= -p(t)(-2cY + 2v(t)A), \\ \dot{p}(t)Y &= -p(t)(2cX - 2u(t)A). \end{aligned}$$

Letting $a(t) := p(t)A$, $x(t) := p(t)X$ and $y(t) := p(t)Y$ this reads

$$(14) \quad \begin{bmatrix} \dot{a} \\ \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -2uy + 2vx \\ 2cy - 2va \\ -2cx + 2ua \end{bmatrix} = 2 \begin{bmatrix} 0 & v & -u \\ -v & 0 & c \\ u & -c & 0 \end{bmatrix} \begin{bmatrix} a \\ x \\ y \end{bmatrix}$$

which implies that $a(t)^2 + x(t)^2 + y(t)^2$ is constant. Note that (14) holds irrespectively of the choice of the penalty function Φ . This choice, however, determines how the optimal controls u and v can be expressed in terms of the functions a , x and y , as will be discussed now.

Energy-optimal control

Let us choose $\Phi(u, v) := (1/2) \cdot (u^2 + v^2)$. We want to first rule out the abnormal case $\chi = 0$. Assume $\chi = 0$; then the absence of constraints on the controls u and v ensures that $x \equiv 0$ and $y \equiv 0$. Plugging this into (14) yields $\dot{a} = 0$, $0 = -2va$ and $0 = 2ua$. Hence a is a constant; in fact a nonzero constant, because otherwise we would have $p \equiv 0$. But then $u \equiv 0$ and $v \equiv 0$, which yields a solution only if the uncontrolled system automatically reaches the desired state at time τ , a trivial case which can be discarded. Hence we may assume $\chi = 1$ so that the Hamiltonian (12) becomes

$$(15) \quad H = (1/2) \cdot (u^2 + v^2) + ca(t) + ux(t) + vy(t).$$

Minimization of (15) with respect to u and v results in

$$(16) \quad u(t) = -x(t), \quad v(t) = -y(t).$$

Plugging this into (14) yields $\dot{a} = 0$ (so that a is a constant) and then $\dot{x} = 2(c+a)y$ and $\dot{y} = -2(c+a)x$, which implies that there are a constant r and a function φ such that $x(t) = r \cos(\varphi(t))$ and $y(t) = r \sin(\varphi(t))$ and $\dot{\varphi} = -2(c+a)$, i.e.,

$$(17) \quad \varphi(t) = \varphi_0 - 2(c+a)t.$$

Hence the optimal trajectory satisfies $\dot{U}(t) = \Theta(t)U(t)$ where

$$(18) \quad \begin{aligned} \Theta(t) &:= cA + r \cos(\varphi(t))X + r \sin(\varphi(t))Y \\ &= c \begin{bmatrix} i & 0 \\ 0 & -i \end{bmatrix} + r \begin{bmatrix} 0 & -e^{-i\varphi} \\ e^{i\varphi} & 0 \end{bmatrix}; \end{aligned}$$

it remains to adjust the constants a , r and φ_0 in such a way that the desired change from $U(0) = \mathbf{1}$ to $U(\tau)$

is effected. We now use a trick to convert the equation $\dot{U} = \Theta U$ (which is a linear differential equation with time-varying coefficients) into a linear differential equation with constant coefficients by introducing the function $t \mapsto T(t) \in \text{SU}(2)$ defined by

$$(19) \quad T := \frac{1}{\sqrt{2}} \begin{bmatrix} e^{i\varphi/2} & -e^{-i\varphi/2} \\ e^{i\varphi/2} & e^{-i\varphi/2} \end{bmatrix}.$$

We observe that both

$$(20) \quad T \begin{bmatrix} i & 0 \\ 0 & -i \end{bmatrix} T^{-1} = \begin{bmatrix} 0 & i \\ i & 0 \end{bmatrix} = Y$$

and

$$(21) \quad T \begin{bmatrix} 0 & -e^{-i\varphi} \\ e^{i\varphi} & 0 \end{bmatrix} T^{-1} = \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} = X$$

are constant in time, which is also true of

$$(22) \quad \dot{T}T^{-1} = \frac{\dot{\varphi}}{2} \begin{bmatrix} 0 & i \\ i & 0 \end{bmatrix} = -(c+a) \cdot Y.$$

Thus the function

$$(23) \quad V(t) := T(t)U(t)$$

satisfies

$$(24) \quad \begin{aligned} \dot{V} &= \dot{T}U + T\dot{U} = \dot{T}U + T\Theta U \\ &= (\dot{T}T^{-1} + T\Theta T^{-1})TU \\ &= (\dot{T}T^{-1} + T\Theta T^{-1})V \\ &= -(c+a)Y + cY + rX)V \\ &= (rX - aY)V, \end{aligned}$$

which has constant coefficients; in fact, letting $z := r - ia$, this equation simply reads

$$(25) \quad \dot{V}(t) = A_z V(t) \quad \text{where } A_z := \begin{bmatrix} 0 & -\bar{z} \\ z & 0 \end{bmatrix}$$

which can be explicitly solved, using $U(0) = \mathbf{1}$, to yield

$$(26) \quad \begin{aligned} V(t) &= \exp(tA_z)V(0) \\ &= \frac{1}{\sqrt{2}} \exp(tA_z) \begin{bmatrix} e^{i\varphi_0/2} & -e^{-i\varphi_0/2} \\ e^{i\varphi_0/2} & e^{-i\varphi_0/2} \end{bmatrix}. \end{aligned}$$

Introducing the abbreviations

$$(27) \quad \alpha := \varphi_0/2 \quad \text{and} \quad \beta := \varphi(\tau)/2 = \alpha - (c+a)\tau$$

and using the fact that $U(t) = T(t)^{-1}V(t) = T(t)^*U(t)$, this yields

$$(28) \quad U(t) = \frac{1}{2} \begin{bmatrix} e^{-i\beta} & e^{-i\beta} \\ -e^{i\beta} & e^{i\beta} \end{bmatrix} \exp(tA_z) \begin{bmatrix} e^{i\alpha} & -e^{-i\alpha} \\ e^{i\alpha} & e^{-i\alpha} \end{bmatrix}.$$

Using (9) with $c = 0$ at the final time $t = \tau$, we find that

$$(29) \quad \exp(\tau A_z) = \begin{bmatrix} C & -\bar{S} \\ S & C \end{bmatrix}$$

where

$$(30) \quad C := \cos(\tau|z|) \quad \text{and} \quad S := \frac{z}{|z|} \sin(\tau|z|);$$

a subsequent evaluation of (28) then yields

$$(31) \quad U(\tau) = \begin{bmatrix} e^{i(\alpha-\beta)}(C+i\text{Im}S) & -e^{-i(\alpha+\beta)} \cdot \text{Re}S \\ e^{i(\alpha+\beta)} \cdot \text{Re}S & e^{i(\beta-\alpha)}(C-i\text{Im}S) \end{bmatrix}.$$

Denoting by U_{ij} the entries of $U(\tau)$, we see from (31) that $e^{i(\beta-\alpha)}U_{11} = C + i \cdot \text{Im}S$; thus if P is the polar angle of $U_{11} \in \mathbb{C}$ (so that $U_{11} = |U_{11}|e^{iP}$) we have

$$(32) \quad |U_{11}|e^{i(\beta-\alpha+P)} = C + i \cdot \text{Im}S.$$

Letting

$$(33) \quad \theta := -a\tau, \quad \theta_0 := c\tau - P, \quad w := \tau|z| = \tau\sqrt{r^2+a^2}$$

(where θ_0 is a known constant whereas θ and w are unknowns because a and r are) we have $\theta - \theta_0 = P - (c+a)\tau = P + \beta - \alpha$; hence (32) takes the form

$$(34) \quad |U_{11}| \cdot \begin{bmatrix} \cos(\theta - \theta_0) \\ \sin(\theta - \theta_0) \end{bmatrix} = \begin{bmatrix} \cos(w) \\ \theta \cdot \sin(w)/w \end{bmatrix}.$$

Taking norms on both sides of (32) we find that $|U_{11}|^2 = \cos(w)^2 + \theta^2 \sin(w)^2/w^2$ and hence that

$$(35) \quad \theta = \frac{\varepsilon w \sqrt{|U_{11}|^2 - \cos^2 w}}{\sin w}$$

where $\varepsilon \in \{\pm 1\}$. Furthermore, (34) implies that $\tan(\theta - \theta_0) = \theta \tan(w)/w$ and hence that

$$(36) \quad \tan \left[\frac{\varepsilon w \sqrt{|U_{11}|^2 - \cos^2 w}}{\sin w} - \theta_0 \right] = \frac{\varepsilon \sqrt{|U_{11}|^2 - \cos^2 w}}{\cos w}.$$

This equation has more than one solution, but since the control effort is given by

$$(37) \quad \begin{aligned} \int_0^\tau \Phi(u, v) dt &= \int_0^\tau \frac{u^2 + v^2}{2} dt = \frac{r^2\tau}{2} \\ &= \frac{\tau}{2} \left(\frac{w^2}{\tau^2} - a^2 \right) = \frac{w^2 - \tau^2 a^2}{2\tau} \\ &= \frac{w^2 - \theta^2}{2\tau} = \frac{1 - |U_{11}|^2}{2\tau} \frac{w^2}{\sin^2 w}, \end{aligned}$$

we are looking, amongst all possible solutions, for the one for which $|w/\sin(w)|$ is minimal. Once (36) has been solved for w , we plug the result into (35) to obtain θ ,

then let $a := -\theta/\tau$ and $r := \sqrt{(w/\tau)^2 - a^2}$ according to (33); finally, φ_0 can be determined from

$$(38) \quad -\frac{U_{21}}{U_{12}} = e^{2i(\alpha+\beta)} = e^{2i(\varphi_0 - c\tau - a\tau)}.$$

Once a, r and φ_0 are found, the optimal controls are given by

$$(39) \quad \begin{aligned} u(t) &= -x(t) = -r \cdot \cos(\varphi_0 - 2(c+a)t), \\ v(t) &= -y(t) = -r \cdot \sin(\varphi_0 - 2(c+a)t). \end{aligned}$$

The special case $U_{11} = 0$ is particularly simple. In this case necessarily $|U_{12}| = 1$, say $U_{12} = e^{i\sigma}$. Equation (34) implies that $\cos(w) = 0$ and $\theta = 0$, hence $a = 0$ and $w = \tau r$; the equation $\cos(w) = 0$ thus yields $\tau r = (\pi/2) + k\pi$ with $k \in \mathbb{Z}$. Finally, equation (38) becomes $e^{2i\sigma} = e^{2i\varphi_0 - 2c\tau}$ so that $\varphi_0 = \sigma + c\tau$. (Note that φ_0 enters the control law only modulo 2π .) The value k has to be chosen to make $|r|$ as small as possible; since one of the choices $k = 0$ and $k = -1$ always gives a solution, we find that

$$(40) \quad \begin{aligned} u(t) &= \varepsilon \cdot \frac{\pi}{2\tau} \cos(\sigma + c\tau - 2ct), \\ v(t) &= \varepsilon \cdot \frac{\pi}{2\tau} \sin(\sigma + c\tau - 2ct), \end{aligned}$$

where $\varepsilon \in \{\pm 1\}$ in (40) must be chosen in such a way that the resulting trajectory $t \mapsto U(t)$ leads to the desired state $U(\tau)$.

Time-optimal control: First case

We now consider the question of time-optimal control (i.e., with the cost function $\Phi(u, v) = 1$) under the constraint $u^2 + v^2 \leq 1$. In this case minimization of (12) yields

$$(41) \quad u = \frac{-x}{\sqrt{x^2 + y^2}}, \quad v = \frac{-y}{\sqrt{x^2 + y^2}}.$$

Plugging this into (14) results in $\dot{a} = 0$ (so that a is constant) and the system

$$(42) \quad \begin{aligned} \dot{x} &= 2cy + 2ay/\sqrt{x^2 + y^2} \\ \dot{y} &= -2cx - 2ax/\sqrt{x^2 + y^2} \end{aligned}$$

from which we conclude that $x\dot{x} + y\dot{y} = 0$, i.e., that $x^2 + y^2$ is constant. Hence there exist a constant r and a function Φ such that $x(t) = r \cos(\Phi(t))$ and $y(t) = r \sin(\Phi(t))$ which, when plugged back into (42), yields $\dot{\Phi} = -2(c + (a/r))$ and hence that

$$(43) \quad \Phi(t) = \Phi_0 - 2 \left(c + \frac{a}{r} \right) t.$$

We see that this solution is completely analogous to the one found in the energy-optimal case; we simply have to replace a by a/r . (Consequently, the time-optimal control

under the given constraint can be found by solving, for a given $\tau > 0$, the solution for the energy-optimal problem and then selecting the smallest τ for which the solution found is compatible with the constraint $u^2 + v^2 \leq 1$.)

Time-optimal control: Second case

We consider again the case $\Phi(u, v) = 1$ (i.e., the case of time-optimal control), but this time with the individual control constraints $|u| \leq 1$ and $|v| \leq 1$ instead of the more severe overall constraint $u^2 + v^2 \leq 1$. In this case minimization of (12) yields

$$(44) \quad u(t) = -\text{sign}(x(t)) \quad \text{and} \quad v(t) = -\text{sign}(y(t))$$

unless there is an interval on which $x \equiv 0$ or $y \equiv 0$ (in which case u or v could not be determined on this interval from minimizing (12)). Let us show that this is only possible if both $u \equiv 0$ and $v \equiv 0$, so that the only possible singular arcs are drift arcs (also called coast arcs) during which no control whatsoever is applied). (It will become clear from the subsequent discussion that generically those arcs do not occur and can be ignored as far as practical implementation of an optimal control scheme is concerned.) Assume that $x \equiv 0$ on some time interval. Then, according to (14), on this time interval the following equations hold:

$$(45) \quad \begin{bmatrix} \dot{a} \\ \dot{y} \end{bmatrix} = 2u \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}, \quad va = cy.$$

Denoting by U an antiderivative of u and letting $C(t) := \cos(2U(t))$ and $S(t) := \sin(2U(t))$, we find from the first equation in (45) that

$$(46) \quad \begin{bmatrix} a(t) \\ y(t) \end{bmatrix} = \begin{bmatrix} C(t) & -S(t) \\ S(t) & C(t) \end{bmatrix} \begin{bmatrix} a_0 \\ y_0 \end{bmatrix}.$$

Apart from the trivial cases $a_0 = y_0 = 0$ and $U(t) = \text{const}$, this implies (because of the second equation in (45)) that

$$(47) \quad v(t) = c \cdot \frac{y(t)}{a(t)} = c \cdot \frac{a_0 S(t) + y_0 C(t)}{a_0 C(t) - y_0 S(t)}$$

is not constant on any part of the time interval considered, which is only possible if $y \equiv 0$ on this interval. But then $x \equiv 0$ and $y \equiv 0$ on this interval, which (as we saw in the discussion preceding (15)) implies $u \equiv 0$ and $v \equiv 0$. Let us discuss the two trivial cases mentioned before. If $a_0 = y_0 = 0$ then (46) implies $y \equiv 0$, and we again obtain $x = y = 0$ and hence $u = v = 0$. If U is constant, then $u \equiv 0$, hence a and y are also constant. The Hamiltonian is then given by $H = ca + vy$. The fact that the Hamiltonian is zero along an optimal trajectory, together with the second equation in (45), gives rise to the equation

$$(48) \quad \begin{bmatrix} v & -c \\ c & v \end{bmatrix} \begin{bmatrix} a \\ y \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

and hence that $a = y = 0$ and hence $u = v = 0$ again.

Ignoring coast arcs for the time being, the time interval $[0, \tau]$ splits into intervals on which both u and v are constant with values in $\{\pm 1\}$. On each such interval equation (14) becomes

$$(49) \quad \begin{bmatrix} \dot{a} \\ \dot{x} \\ \dot{y} \end{bmatrix} = 2 \begin{bmatrix} 0 & v & -u \\ -v & 0 & c \\ u & -c & 0 \end{bmatrix} \begin{bmatrix} a \\ x \\ y \end{bmatrix}$$

which is an equation with constant coefficients which can be explicitly integrated as

$$(50) \quad \begin{bmatrix} a(t) \\ x(t) \\ y(t) \end{bmatrix} = \exp \left(2(t-s) \begin{bmatrix} 0 & v & -u \\ -v & 0 & c \\ u & -c & 0 \end{bmatrix} \right) \begin{bmatrix} a(s) \\ x(s) \\ y(s) \end{bmatrix}$$

where the exponential can be computed using the Rodrigues formula which states that for any skew-symmetric matrix

$$(51) \quad L(\omega) = \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix}$$

where $\omega = (\omega_1, \omega_2, \omega_3)^T \in \mathbb{R}^3$ the exponential $\exp(L(\omega))$ is given by

$$(52) \quad (\cos \|\omega\|)\mathbf{1} + \frac{1 - \cos \|\omega\|}{\|\omega\|^2} \omega \otimes \omega + \frac{\sin \|\omega\|}{\|\omega\|} L(\omega).$$

Thus if $[s, t]$ is a time interval during which u and v are constant we have $\omega = -2(c, u, v)^T$ and hence

$$(53) \quad \begin{bmatrix} a(t) \\ x(t) \\ y(t) \end{bmatrix} = \exp \left(2(t-s) \begin{bmatrix} 0 & v & -u \\ -v & 0 & c \\ u & -c & 0 \end{bmatrix} \right) \begin{bmatrix} a(s) \\ x(s) \\ y(s) \end{bmatrix}$$

where the exponential is given by

$$(54) \quad \begin{aligned} & \cos(2(t-s)\sqrt{c^2+2}) \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \\ & + \frac{1 - \cos(2(t-s)\sqrt{c^2+2})}{c^2+2} \begin{bmatrix} c^2 & uc & vc \\ uc & 1 & uv \\ vc & uv & 1 \end{bmatrix} \\ & + \frac{\sin(2(t-s)\sqrt{c^2+2})}{\sqrt{c^2+2}} \begin{bmatrix} 0 & v & -u \\ -v & 0 & c \\ u & -c & 0 \end{bmatrix}. \end{aligned}$$

Let us note that the motion of the vector $(a, x, y)^T$ during the time interval $[s, t]$ is a rotation with constant angular velocity $\sqrt{c^2+2}$ about the axes pointing in the direction of $(c, u, v)^T$; hence

$$(55) \quad 2(t-s)\sqrt{c^2+2} = 2\Phi_{t,s}$$

where $\Phi_{t,s}$ is the angle swept out by this vector.

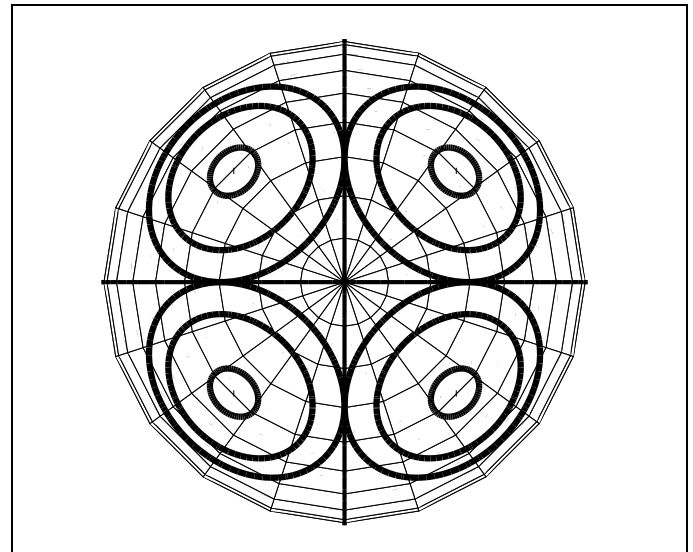


Fig. 1: Evolution of adjoint variables.

Depending on the four possibilities $(u, v) = (\pm 1, \pm 1)$, there are four possible axes of rotation; the larger $|c|$, the closer these axes are towards the a -axis in the adjoint space. The diagram shows a view from top (i.e., from the positive a -axis) onto the xy -plane. The adjoint variables evolve on a sphere $a^2 + x^2 + y^2 = R^2$; around each of the four axes there is a circle which touches both the plane $x = 0$ and the plane $y = 0$. If (a_0, x_0, y_0) lies in the interior of any such circle, no switching can occur, because then the trajectory $t \mapsto (a(t), x(t), y(t))$ can never leave the quadrant in which it starts. The exterior of the union of these four circles is composed of two regions; region I containing the point $(R, 0, 0)$, region II containing the point $(0, 0, R)$. If $c < 0$ the positively oriented rotation axes “stick out” of the diagram, so that the motion along the circles is in the mathematically positive sense. Thus if (a_0, x_0, y_0) is in region I, we follow the switching pattern

u	-1	-1	1	1
v	-1	1	1	-1

(traversing the four quadrants of the xy -plane in clockwise fashion), whereas if (a_0, x_0, y_0) is in region II, we follow the switching pattern

u	-1	1	1	-1
v	-1	-1	1	1

(traversing the four quadrants in a counterclockwise fashion). This motion in the adjoint space needs to be strictly distinguished from the associated motion in the state space $SU(2)$ which is determined from the switching pattern by the fact that on each time interval on which u and v are constant the state equation (1) becomes

$$(56) \quad \dot{U}(t) = \begin{bmatrix} ci & -u + iv \\ u + iv & -ci \end{bmatrix} U(t)$$

which is also an equation with constant coefficients and hence can be explicitly integrated via

$$(57) \quad U(t) = \exp\left((t-s) \begin{bmatrix} ci & -u+iv \\ u+iv & -ci \end{bmatrix}\right) U(s)$$

where the exponential can be evaluated using (9). The remaining step is to determine the control synthesis (yielding for each desired target state the times at which switchings in the optimal control functions occur), which in particular requires deriving an upper bound for the number of possible switchings. This is not a trivial task and will be described in a subsequent paper. Possible approaches are the symplectic techniques developed by Agrachev et al. (see [1], [2]) or Sussmann's envelope method (see [5], [6]), but in our problem a simpler approach is possible because reduction to a two-dimensional problem is possible, as follows. Consider the Hopf map, i.e., the mapping $\Phi : \text{SU}(2) \rightarrow \mathbb{S}^2$ given by

$$(58) \quad \begin{bmatrix} B & -\overline{C} \\ C & \overline{B} \end{bmatrix} \mapsto \begin{bmatrix} \xi_1 \\ \xi_2 \\ \xi_3 \end{bmatrix} := \begin{bmatrix} -2 \text{Im}(\overline{B}C) \\ 2 \text{Re}(\overline{B}C) \\ |B|^2 - |C|^2 \end{bmatrix}.$$

(This is really a mapping into \mathbb{S}^2 because $\xi_1^2 + \xi_2^2 + \xi_3^2 = 4|\overline{B}C|^2 + (|B|^2 - |C|^2)^2 = (|B|^2 + |C|^2)^2 = 1$.) Note that the system dynamics (1) can be rewritten as

$$(59) \quad \begin{aligned} \dot{B} &= ciB - uC + viC \\ \dot{C} &= -ciC + uB + viB \end{aligned}$$

which, when plugged into (58), yields

$$(60) \quad \begin{bmatrix} \dot{\xi}_3 \\ \dot{\xi}_1 \\ \dot{\xi}_2 \end{bmatrix} = 2 \begin{bmatrix} 0 & v & -u \\ -v & 0 & c \\ u & -c & 0 \end{bmatrix} \begin{bmatrix} \xi_3 \\ \xi_1 \\ \xi_2 \end{bmatrix},$$

an equation which coincides with the adjoint equation (14). Since (60) is a control system evolving on a two-dimensional manifold, the techniques described in [4] are applicable to determine an upper bound for the number of switchings for the optimal controls in (60). Now if $t \mapsto u(t)$ and $v \mapsto v(t)$ are controls which optimally steer system (60) from ξ_0 to ξ_1 in time τ and if $t \mapsto g(t)$ is any trajectory in $\text{SU}(2)$ resulting from these controls, then this latter trajectory is automatically an optimal trajectory joining the initial state $g(0)$ to the final state $g(\tau)$. This simple observation can then be used to derive an upper bound for the number of control switchings for system (1) in terms of those for system (60); cf. [4] in which this technique was applied to a system without drift.

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