

Symbolic equation for linear analog electrical circuits using Matlab

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Abstract: - In this paper is presented a program which generates the modified nodal equation for electric analog circuits in a symbolic, partial symbolic and numerical mode. The program is an application, made in the environment of the program MATLAB version 7.1, which has a powerful symbolic math toolbox. MATLAB is a high-performance software package dedicated for numerical analysis and graphic representations in engineering applications. In this paper we try to explore the capabilities of this program in symbolic domain.

Key-Words: - analog circuits, circuit functions, symbolic equations, Matlab, netlist, modified nodal analysis.

1 Introduction

The modified nodal methods have been implemented in a program on a Pentium Dual Core computer compatible to obtain symbolic forms, partly symbolic or numerical equations for electronic linear analog circuits. Between the input gate and the output one specified by the user, any of the four types of circuit functions (transfer impedance - Z_{ei} , admittance transfer function - Y_{ei} , voltage transfer factor (amplifier) - A_{ei} and current

transfer factor (amplifier) - B_{ei}) for linear analog electric circuits around a functionary point. Starting from the description of the circuit through to a file-type input netlist, according to the window shown in figure 1, the following capabilities:

- generates symbolic, partly symbolic or numerical equations using modified nodal analysis for linear electrical circuits;
- generates symbolic form of the extensive matrix of the system equations and determines the symbolic solution, partly symbolic or numerical

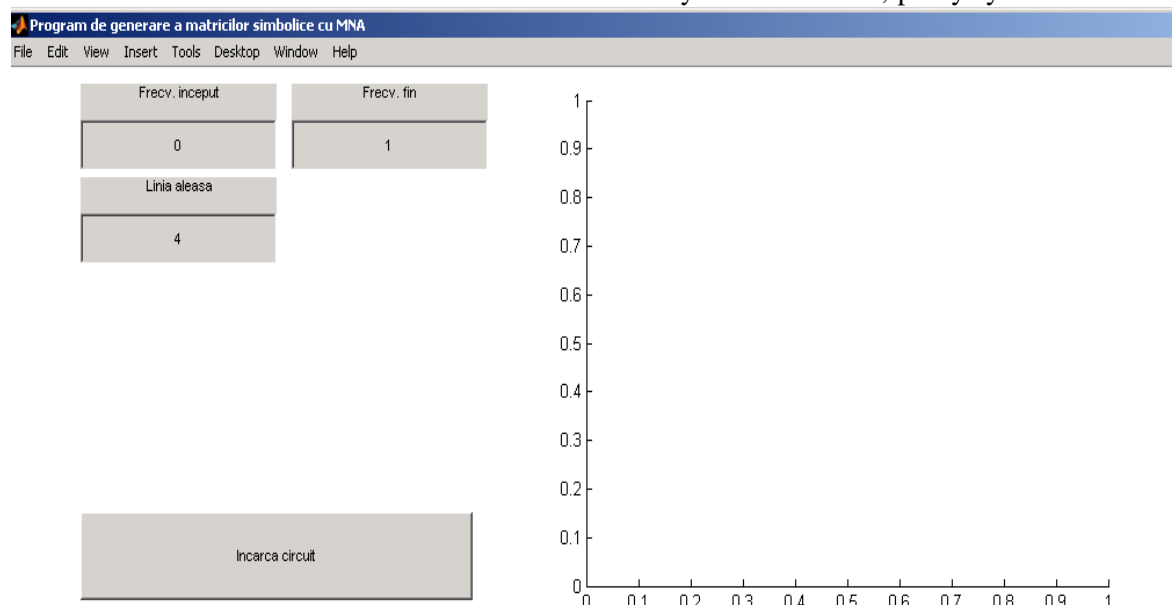


Fig.1 Application window

to the circuit system;

Data entry is a set of lines describing n_l circuit branch. Each branch of the circuit is described by a proper letter which indicates the type of circuit elements, the first node, final node, the nominal value and the value of the tolerance. In the case of controlled sources we should also introduce nodes of command branch. The netlist is similar to those described in the program SPICE.

2 Modified Nodal Analysis (MNA)

To solve the circuit and obtain the desired circuit function we use the modified nodal analysis.

In the modified nodal analysis the circuit matrix is obtained by the augmentation of the nodal conductance (admittance) matrix corresponding to the NA-compatible circuit elements with additional rows and columns for non-NA-compatible circuit elements.

The circuit equations in operational corresponding to the modified nodal analysis method, have the following form:

$$\begin{bmatrix} \mathbf{Y}_{n-1,n-1}(s) & \mathbf{B}_{n-1,m}(s) \\ \mathbf{A}_{m,n-1}(s) & \mathbf{Z}_{m,m}(s) \end{bmatrix} \cdot \begin{bmatrix} \mathbf{V}_{n-1}(s) \\ \mathbf{I}_m(s) \end{bmatrix} = \begin{bmatrix} \mathbf{I}_{sc,n-1}(s) \\ \mathbf{E}_m(s) \end{bmatrix}, (1)$$

Where: $\mathbf{Y}_{n-1,n-1}(s)$ - is the admittance matrix corresponding to the $n-1$ independent nodes; $\mathbf{B}_{n-1,m}(s)$ is an $(n-1) \times m$ matrix and it contains the

elements $-1, 0, +1$ and the current gains of the CCCS's; $\mathbf{A}_{m,n-1}(s)$ is an $m \times (n-1)$ matrix

containing the elements $-1, 0, +1$ and the voltage gains of the VCVS's; $\mathbf{Z}_{m,m}(s)$ is a $m \times m$ matrix having the transfer impedances of the CCVS's; $\mathbf{V}_{n-1}(s)$ is node voltage vector corresponding to the $n-1$ independent nodes. The vector $\mathbf{I}_m(s)$ represents the current vector corresponding to the non-NA compatible circuit branches and it has the following structure:

$$\mathbf{I}_m(s) = \left[(\mathbf{I}_e(s))^t, (\mathbf{I}_{e_c}(s))^t, (\mathbf{I}_{e_c}(s))^t, (\mathbf{I}_{j_c}(s))^t, (\mathbf{I}_L(s))^t \right]^t, (2)$$

where : $(\mathbf{I}_e(s))^t$ is the ideal voltage source current vector; $(\mathbf{I}_{e_c}(s))^t$ the controlled (output) branch current vector of all controlled voltage sources; $(\mathbf{I}_{e_c}(s))^t$ the controlling (input) branch current vector of the CCVS's; $(\mathbf{I}_{j_c}(s))^t$ the controlling branch current vector of the CCCS's. The vectors $\mathbf{I}_{sc,n-1}(s)$ and $\mathbf{E}_m(s)$ represent the contributions of the excitation sources (independent current and voltage sources).

3 Description of the application

To explain and understand this application we consider the following circuit (figure 2). This

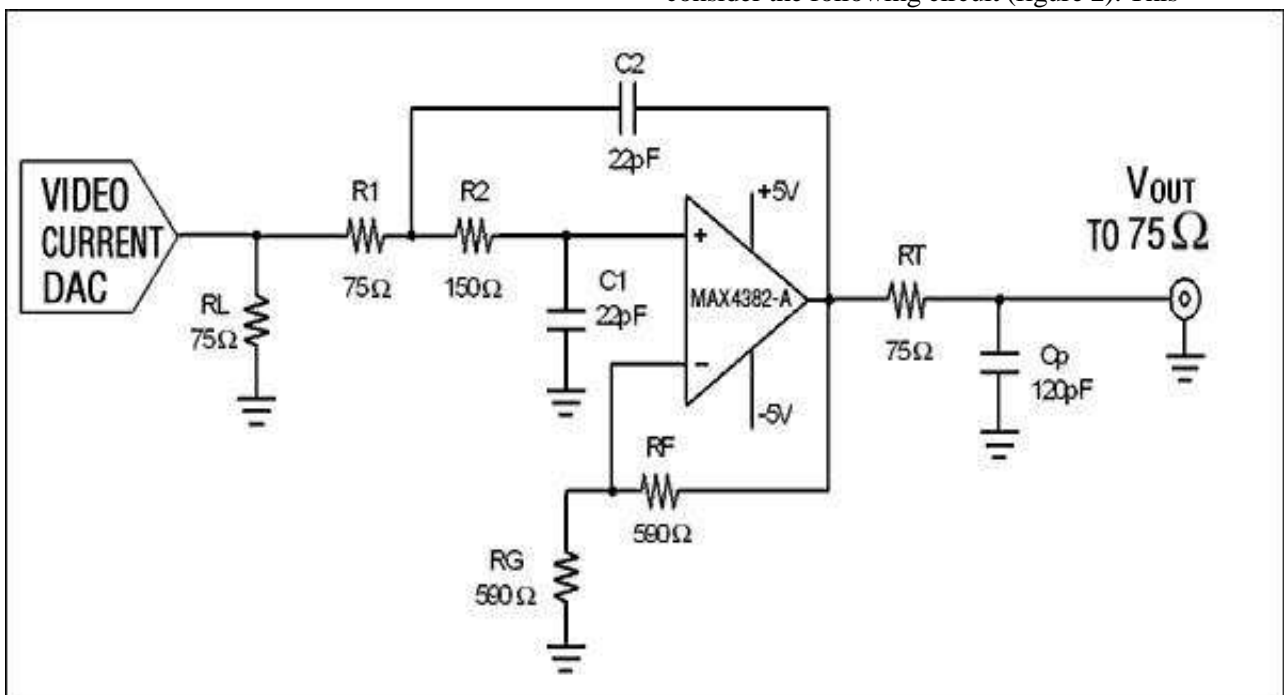


Fig. 2 Lowpass Sallen Key filter

application describes how to use a lowpass Sallen-Key filter with a dual supply voltage. The circuit provides a Butterworth response with a 30MHz bandwidth, and is ideal for video-reconstruction filtering in HDTV applications. In HDTV applications, lowpass filters are used for reconstruction of RGB and component video (Y, Pb, and Pr) signals. They are placed following the video DAC to remove the higher frequency replicas of the signals, as well as before the ADC for anti-aliasing. Figure 2 shows a one-channel, dual-supply configuration incorporating the MAX4382. It is a three-pole, Sallen-Key Butterworth lowpass filter, in which the current DAC generates the video signal, and the resistor (RL) sets the amplitude. With the MAX4382, the RL, R1, R2, C1, and C2 form a two-pole, Sallen-Key lowpass filter having a gain of 2. The driving load (75Ω) at the output, plus RT and Cp, sets the real pole.

In the Figure 2 circuit, the -3dB bandwidth is about 30MHz. The attenuation is approximately 14dB at 44.25MHz, and 28dB at 74.25MHz. The group delay is roughly 6.5ns. If the current DAC load is different than 75Ω, just use the following relationship to set the value of R1: $R1 + RL = 150\Omega$. For RL greater than 150Ω, C1, C2, R1, and R2 will need to be adjusted.

The input file for this example has the following structure:

```
6
R1 1 0 75 0.02
R2 1 2 75 0.02
R3 2 3 150 0.02
R4 5 0 590 0.02
R5 6 5 590 0.02
R6 6 4 75 0.02
Rf 3 5 100000 0.00001
C1 3 0 0.000000000022 0.1
C2 2 6 0.000000000022 0.1
C3 4 0 0.000000000120 0.1
E1 1 0 1 0.1
G1 3 5 0 6 1000000
```

The first row from this net list file represents the number of nodes of the circuit. After that each line describes a circuit element which is defined by the first letter (ex. R for resistor, C for capacitor etc). This application, in order to solve the circuit with symbolic method, needs to contain the following instruction lines, particularized for each circuit element – in the example we have the code for resistors.

```
for i = 1:n
%daca avem resistor
    if (findstr(latura(i).tip, 'R') == 1)
        nr_r_k = nr_r_k + 1;
        k1 = int8(str2double(num2str(latura(i).ni)));
        k2 = int8(str2double(num2str(latura(i).nf)));
        if ((k1 > 0) & (k2 > 0))
            exp1 = [A(k1, k1) '1/' latura(i).tip];
            exp2 = [A(k1, k2) '-1/' latura(i).tip];
            exp3 = [A(k2, k1) '-1/' latura(i).tip];
            exp4 = [A(k2, k2) '1/' latura(i).tip];
            str1 = sym(exp1);
            str2 = sym(exp2);
            str3 = sym(exp3);
            str4 = sym(exp4);
            C(k1, k1) = C(k1, k1) + str1;
            C(k1, k2) = C(k1, k2) + str2;
            C(k2, k1) = C(k2, k1) + str3;
            C(k2, k2) = C(k2, k2) + str4;
```

$$Ae^s \begin{bmatrix} 1/R4 + 1/R2 & -1/R2 & 0 & 0 & 0 & 0 & 1 & 0 \\ -1/R2 & 1/R2 + 1/R3 + s*C2 & -1/R3 & 0 & 0 & -s*C2 & 0 & 0 \\ 0 & -1/R3 & 1/R3 + 1/Rf + s*C1 & 0 & -1/Rf & 0 & 0 & 0 \\ 0 & 0 & 0 & 1/R6 + s*C3 & 0 & -1/R6 & 0 & 0 \\ 0 & 0 & -1/Rf & 0 & 1/R4 + 1/R5 + 1/Rf & -1/R5 & 0 & 0 \\ 0 & -s*C2 & 0 & -1/R6 & -1/R5 & 1/R5 + 1/R6 + s*C2 & 0 & -1 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & A & 0 & -A & -1 & 0 & 0 \end{bmatrix}$$

```
elseif (k1 > 0)
    exp1 = [A(k1, k1) '1/' latura(i).tip];
    str1 = sym(exp1);
    C(k1,k1) = C(k1, k1) + str1;

elseif (k2 > 0)
    exp4 = [A(k2, k2) '1/' latura(i).tip];
    str4 = sym(exp4);
    C(k2, k2) = C(k2, k2) + str4;
end
```

The **A** coefficient matrix obtained with the program for this example will be as above.
The admittance transfer function for this example in a symbolic form:

$$Y_{ei} = \frac{GA(R_5 + R_4)}{(1 + s^2 C_3 R_6) (R_4 R_5 + R_5 R_f + R_4 R_f + R_5 R_3 + R_5 s^2 C_2 R_2 R_3 - R_2 R_5 GA R_f s C_2 + R_2 R_5 R_f s C_2 + R_5 R_f s C_1 R_3 + R_2 R_5 R_f s C_1 + R_2 R_5 R_f s^2 C_1 R_3 C_2 + R_2 R_5 R_3 + R_2 R_f R_4 s C_2 + R_f R_4 s C_1 R_3 + R_2 R_f R_4 s C_1 + R_2 R_f R_4 s^2 C_1 R_3 C_2 + R_2 R_4 s C_2 R_3 + R_4 R_3 + R_2 R_4 GA R_f R_4 + R_2 R_5 s C_2 R_4 + GA R_f s C_1 R_3 R_4 + R_5 s C_1 R_3 R_4 + R_2 GA R_f s C_1 R_4 + R_2 R_5 s C_1 R_4 + R_2 GA R_f s^2 C_1 R_3 C_2 R_4 + R_2 R_5 s^2 C_1 R_3 C_2 R_4) R_f E_1}$$

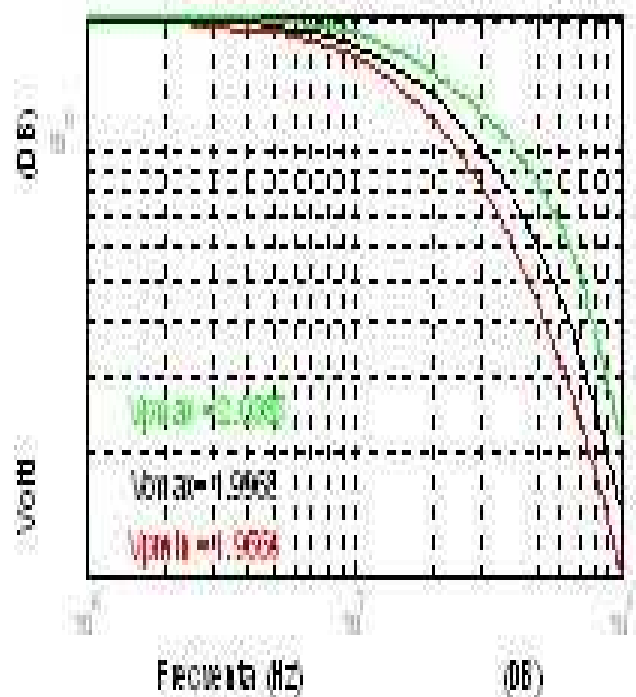


Fig. 3 Waveform for lowpass Sallen-Key filter

In fig. 3 is represented the output waveform for Lowpass Sallen-Key filter obtained with this Matlab application after replacing symbolic values with nominal ones.

4 Examples of applications

Bandpass Sallen-Key filter

The parameter of this filter is Q of 10 and

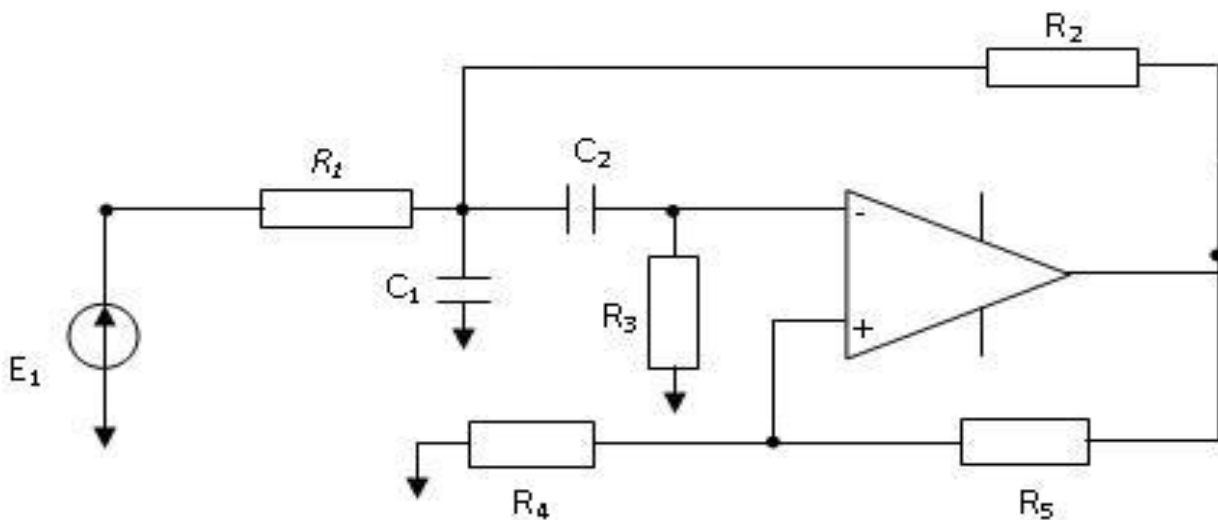


Fig. 4 Bandpass Sallen-Key filter

amplification is 10 at $f_o=500$ Hz. The nominal values of the filter's components are: $R1=15800$; $R2=5110$; $R3=2610$; $R4=3320$; $R5=13300$; $C1=1e-7$; $C2=C1$;

The input file for this example has the following structure:

```

5
R1 1 2 15800 0.02
R2 2 4 5110
C1 2 0 0.00000001 0.1
C2 2 3 0.00000001 0.1
R3 3 0 2610 2

Rf 3 5 10000000000 0.02
R4 5 0 3320 0.02
R5 4 5 13300 0.02
E1 1 0 1
G1 5 3 4 0 10000
    
```

The transfer function for the filter has the following form:

$$Y_e \pm K(s) \frac{C2GA(R5C R4 RfR2R3E1)}{(RfR4R1 C RfR4GAR2C R2R5R3C R4R5R1C R2RfR4 C R5RfR1C R2R3R4s C1R1C R2R3R4s C2R1 C R2R5R3s C1R1C R2R5R3s C2R1C R2R5Rf C R5R3R1C R2R3R4C R4R5R2C s C2R1R2RfR4GA C RfR4GAR2s C2R3C RfR4GAR2s^2 C2R3C1R1 C RfR4GAR2s C1R1C R4R5R2s C2R3 C R4R5s C2R3R1C R4R5R2s^2 C2R3C1R1 C R4R5R2s C1R1 C R4R5R2s C2R1K R5GAR1s C2R3Rf C R2s C2R3RfR4C s C2R3RfR4R1 C R2s^2 C2R3RfR4C1R1C R2R5s C2R3Rf C R5s C2R3RfR1C R2R5s^2 C2R3RfC1R1 C R2RfR4s C1R1C R2RfR4s C2R1C R2R5Rf s C1R1 C R2R5Rf s C2R1C R3R4R1C RfR4GAR1)}$$

The nominal waveform obtained after replacing the symbolic letter with values is illustrated below:

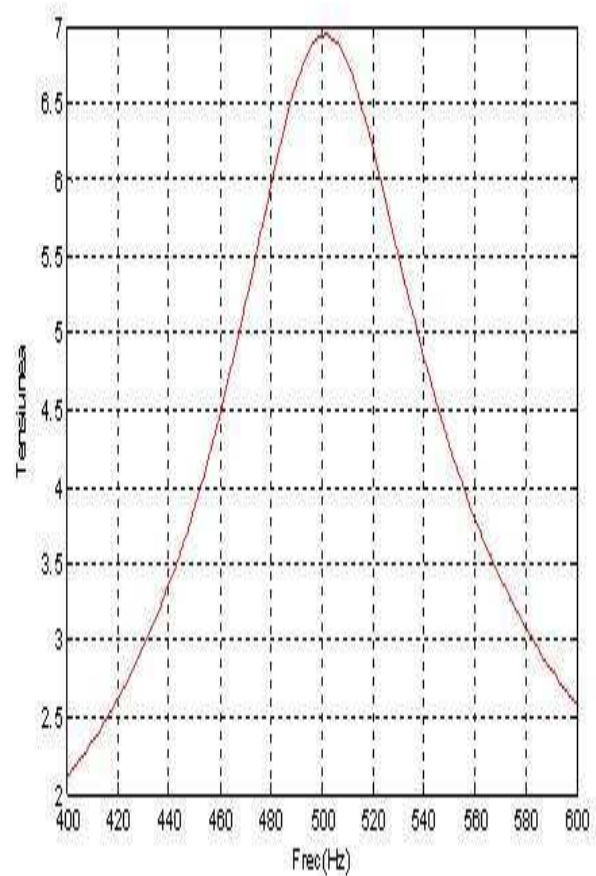


Fig.5 Output waveform for Bandpass Sallen-Key filter

The extend A_{ei} coefficient matrix for this filter is like below:

$$A_{ei} = \begin{bmatrix} 1/R1 & -1/R1 & 0 & 0 & 0 & 0 & 1 & 0 \\ -1/R1 & 1/R1+1/R2+s*C1+s*C2 & -s*C2 & -1/R2 & 0 & 0 & 0 & 0 \\ 0 & -s*C2 & s*C2+1/R3+1/Rf & 0 & -1/Rf & 0 & 0 & 0 \\ 0 & -1/R2 & 0 & 1/R2+1/R5 & -1/R5 & 0 & 1 & 0 \\ 0 & 0 & -1/Rf & -1/R5 & 1/Rf+1/R4+1/R5 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -A & 1 & A & 0 & 0 & 0 \end{bmatrix}$$

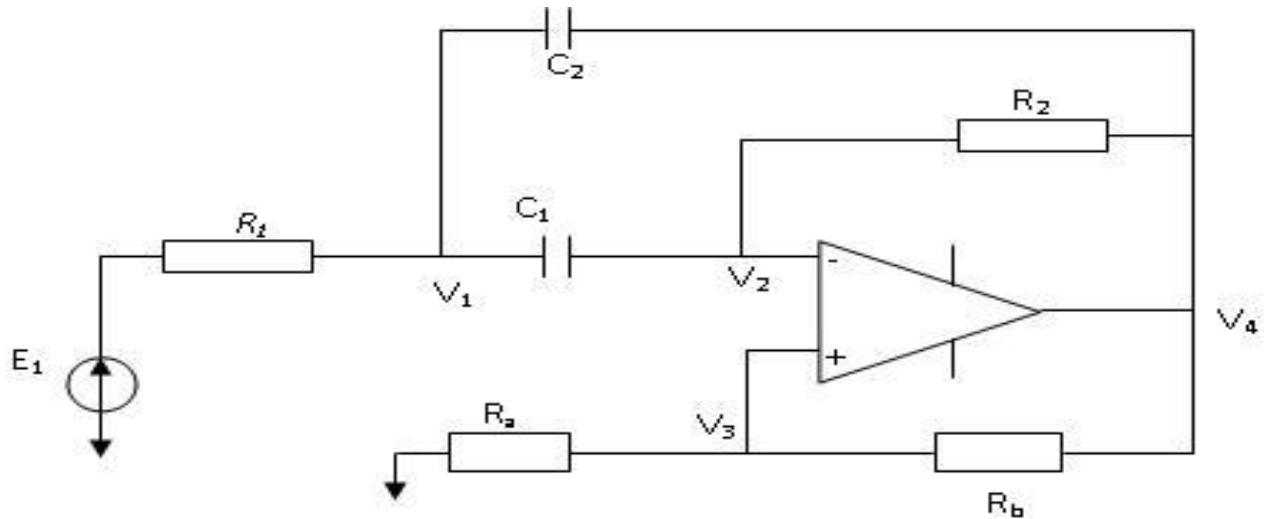


Fig. 7 Bandpass Delyiannis filter

In order to be sure that our application generates correct symbolic equation, and does not introduce some deviation in the comportment of the circuits, we have simulated the same circuit with the same nominal values in ORCAD program, and we obtained the following waveform which is similar, if not identical, with the one obtained with our algorithm.

Bandpass Delyiannis filter

The input data of this bandpass filter are: $f_0 = 500$ Hz; $Q = 20$; $R1 = 4.93K$; $R2 = 205K$; $Ra = 10K$; $Rb = 252K$; $C1 = 0.01\mu F$; $C2 = 0.01\mu F$

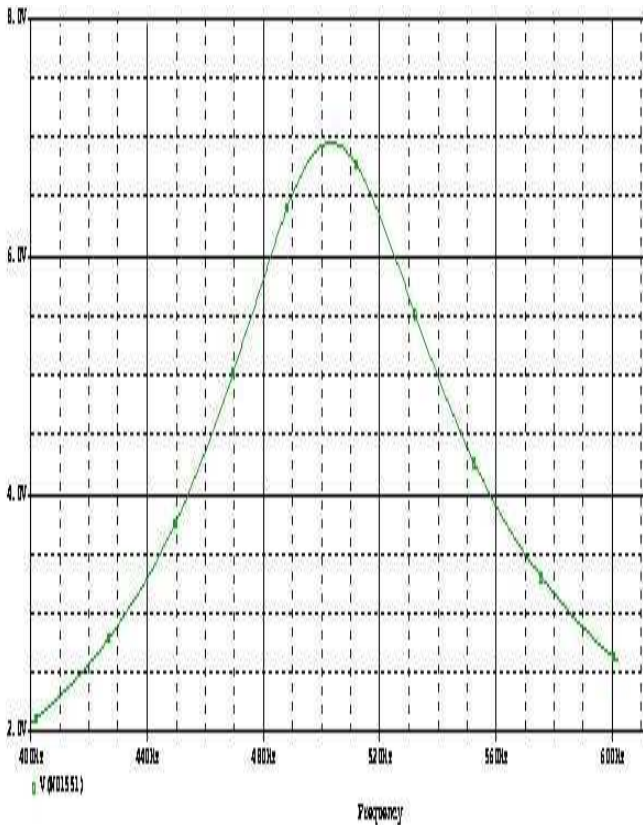


Fig. 6 Output waveform from ORCAD simulation

The input file for this filter has the following structure:

```

5
R1 1 2 4930 0.02
R2 3 4 205000 0.02
C1 2 3 0.000001 0.1
C2 2 4 0.00000001 0.1
R5 3 5 10000 0.2
R3 4 5 252000 0.2
R4 5 0 10000 0.2
E1 1 0 1 0.1
G1 3 5 4 0 1000000
    
```

The transfer function for the filter has the following form:

$$A_{ei} = \begin{bmatrix} 1/R1 & -1/R1 & 0 & 0 & 0 & 0 & 1 & 0 \\ -1/R1 & 1/R1+s*C1+s*C2 & -s*C1 & -s*C2 & 0 & 0 & 0 & 0 \\ 0 & -s*C1 & 1/R2+s*C1+1/R5 & -1/R2 & -1/R5 & 0 & 0 & 0 \\ 0 & -s*C2 & -1/R2 & 1/R2+s*C2+1/R3 & -1/R3 & 0 & 1 & 0 \\ 0 & 0 & -1/R5 & -1/R3 & 1/R5+1/R4+1/R3 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & A & 1 & -A & 0 & 0 & 0 \end{bmatrix}$$

The extend A_{ei} coefficient matrix for this filter is as above.

$$Y_{ei} = (s C1 G A (R4 C R3) R5 R2 E1) / (G A R3 R5 C R5 R4^2 C I R I R2 C K R2 R5 C I R4 G A C R4 R5 C R3 R4 C R5 R3 C R4 R2 C R2 R3 C s C I R I R2 R4 C s C2 R I R2 R4 C R4 R5 C2 R I C s C I R I R2 R3 C s C2 R I R2 R3 C R5 R3 C2 R I C R4 R5 R2 C1 C R2 R3 R4 C I C R2 R5 R3 C I C R4 R5 C I R1 C R3 R4 C I R I C R5 R3 C I R I C^2 C I R I R2 C2 R3 R4 C R2 R5 R3^2 C I G A C2 R I C G A R3 R5 C2 R1 C G A R3 R5 C I R I C R5 R3^2 C I R I R2 C2 C R3 R4 C2 R1)$$

The nominal waveform obtained after replacing the symbolic letter with values is illustrated below:

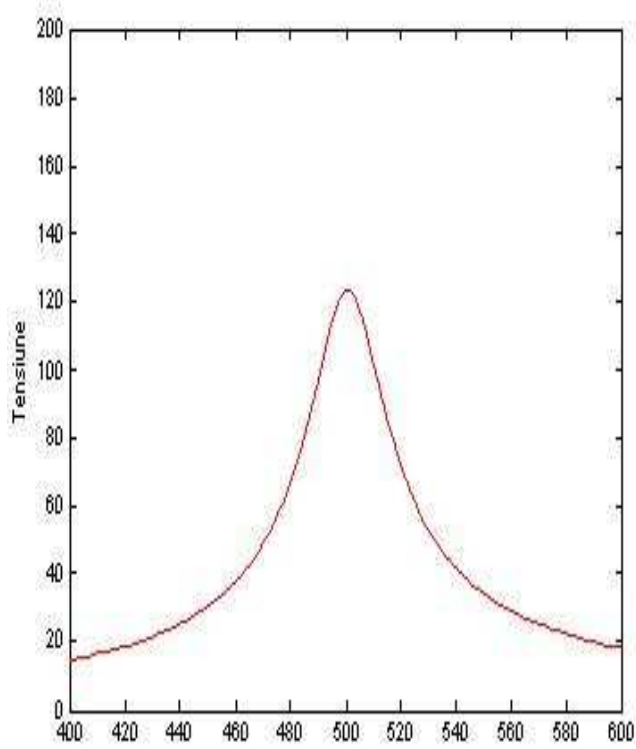


Fig. 8 Output waveform for bandpass Delyiannis filter

In order to be sure that our application generates correct symbolic equation, and does not introduce some deviation in the comportment of the circuits, we have simulated the same circuit with the same nominal values in ORCAD program, and we obtained the following waveform which is similar, if not identical, with the one obtained with our algorithm.

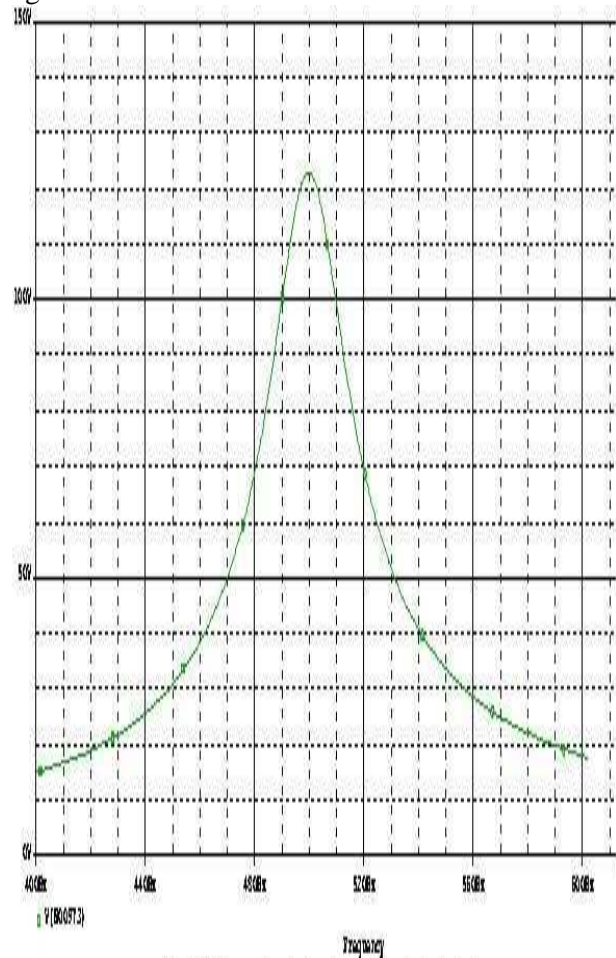


Fig. 9 Output waveform from ORCAD simulation

5 Conclusion

The main advantage of the MNA method is that the contributions of all individual circuit elements can be inserted directly in appropriate places in (1), independently of whether the primary variable of a particular element is a voltage or a current.

MNA method associated with an efficient nod tearing leads to an important reduction in computing time and to an increase of the accuracy.

This is a new software environment that allows the schematic representation, analysis and design for linear analog circuits.

This application is very useful in circuits design because is dedicated only for circuit analysis and combined with the power of Matlab platform we can test very complex circuits.

Next steps are to develop this application with new capabilities like tolerance analysis.

Programs like ORCAD have limited number of circuits nodes that they can solve.

The speed of this application it s not the main issue only the size of the circuit analysis it's important

6 Instruction lines

```
function tolerefectfin
%
clear;
if nargin<1,
    action='start';
end;
%coordonatele ferestrei grafice si a axelor
pe ecran
ps=0.01; %distanța ferestrei fata de stanga
pj=0.3; %distanța ferestrei fata de jos
lg=0.98; %lungimea ferestrei
hg=0.65; %inaltimea ferestrei
global DISP
global maximuri
global count
count=1;
maximuri(count)=0;

DISP=1;
S=brighten([[zeros(8,2) (3:10)/10];
prism(56)],1/3);
if strcmp (action, 'start'),
    clf reset;

set(gcf,'Units','normalized','backingstore','of
f','color',...
```

```
'blue','NumberTitle','off','colormap',S,...
'Position',[.01 .25 .98 .65],...
'Name','ANALIZATOR de
TOLERANTA a CIRCUITELOR
ELECTRICE ANALOGICE');
%colormenu;
end;
n_semn=1; %numarul de tipuri de
semnale
n_buts=n_semn+1; %numarul de butoane
semnal+inchidere
n_butr=4; %numarul de butoane pentru
reprezentari
n_but=n_buts+n_butr+3; % numarul de
butoane
%echivalente (+spatiile)
%se plaseaza butoanele meniului in partea
stinga
h_g1=1-(n_but+1)*.01; %inaltimea
echivalenta pentru butoane
h_but=.9/n_but; %inaltimea butonului
l_but=0.27; %lungimea butonului
d_s1=.01; %distanța fata de marginea
din stanga
d_j1=.01; %distanța fata de marginea
de jos
%se pune butonul de inchidere "stop"
pos = [d_s1 d_j1*.5 l_but h_but]; %pozitia
butonului
%f=figure('Visible','off','Position',[360,500,
450,350]);
hcl = uicontrol (gcf,
'units','normal','pos',pos,...

'String','STOP','Callback',{ @stop_buton_Ca
llback});
%pos = [d_s1 (h_but*(1+n_butr+3)+d_j1)+.015 l_but
h_but-.02];
hincarca=uicontrol(gcf,'units','normal','Style
','pushbutton','String','Incarca
circuit','Position',[d_s1 (h_but*6+d_j1)
l_but .95*h_but],...
'Callback',{ @incarcabutton_Callback});
hfunctie=uicontrol('Style','pushbutton','units
','normal','String','Incarca
functie','Position',[d_s1 (h_but*5+d_j1)
l_but .95*h_but],...
'Callback',{ @functiebutton_Callback});
harunca=uicontrol('Style','pushbutton','units'
,'normal','String','grafic','Position',[d_s1
(h_but*4+d_j1) l_but .95*h_but],...
'Callback',{ @aruncabutton_Callback});
```



```

hgauss = uicontrol (gcf,
'units','normal','position',[d_s1
(h_but*3+d_j1) l_but .95*h_but],...

'String','GAUSS','Callback',{ @distributiebu
tton_Callback});
hsemnal = uicontrol (gcf,
'units','normal','position',[d_s1
(h_but*2+d_j1) l_but .95*h_but],...

'String','semnal','Callback',{ @semnalbutton
_Callback});
hsterge = uicontrol (gcf,
'units','normal','position',[d_s1
(h_but*1+d_j1) l_but .95*h_but],...

'String','sterge','Callback',{ @stergebutton_C
allback});

ha=axes('Units','pixels','Position',[500,50,50
0,485]);

%global SD_AXIS
%SD_AXIS= axes('Position',[1.35*l_but
.15 (1-1.5*l_but) .75]);
%axis off
%set(SD_AXIS,'Position',[1.35*l_but .15
(1-1.5*l_but) .75],...
% 'XColor',[1 0 0],'YColor',[1 0
0],'ZColor',[1 0 0])
% get(SD_AXIS)
%ha=axes('Units','pixels','Position',[50,95,2
00,185]);
rect=[d_s1 ((n_but)*h_but+d_j1) (l_but/2)
h_but-.06];
hfrecin=uicontrol('Style','text','units','normal
','String','Frecv. inceptu','Position',rect);
hf1=uicontrol('Style','edit','units','normal','S
tring','0','units','
normal','Position',[d_s1
((n_but)*h_but+d_j1-0.05) (l_but/2) h_but-
.06]);
hfrecfin=uicontrol('Style','text','units','norma
l','String','Frecv.
fin','Position',[d_s1+l_but/2+.01
((n_but)*h_but+d_j1) (l_but/2) h_but-.06]);
hf2=uicontrol('Style','edit','units','normal','S
tring','1','Position',[d_s1+l_but/2+.01
((n_but)*h_but+d_j1)-0.05 (l_but/2) h_but-
.06]);

%set(f,'Name','Efect toleranta');
set([hincarca,harunca,hfunctie,hfrecin,hf1,h
a,hfrecfin,hf2,hgauss,hsemnal,hsterge],'Unit
s','normalized');

```

```

latura =
struct('tip',{' ','ni',{},'nf',{},'valoare',{},'tole
r',{}});

val(1)=0;
nod1(1)=0;
nod2(1)=0;
frec=[];
functietran=[];
old=-1;

nrlaturi=0;
y=[];
hold on;
% set(f,'Visible','on')

mx=[];

function
incarcabutton_Callback(source,eventdata)

[filename,pathname]=uigetfile('*.cir');

if isequal(filename,0)
disp('Utilizatorul a ales Cancel')
else
disp(['Utilizatorul a
ales',fullfile(pathname,filename)])

%open(file)

fid=fopen(fullfile(pathname,filename),'r');

sir=fgetl(fid);
[mx, sir] = strtok(sir);
nm = str2num(mx)

k=1;
%nm linii matrice

while 1
sir=fgetl(fid);
if ~ischar(sir), break, end

[mx,sir]=strtok(sir);
latura(k).tip=mx;
[mx,sir]=strtok(sir);
latura(k).ni=str2num(mx);
[mx,sir]=strtok(sir);
latura(k).nf=str2num(mx);

```

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